

Operational Calculus (Applied to RC and RL Circuits)

Defining py as $\frac{dy}{dt}$ and $\frac{1}{p}[y]$ as $\int_{-\infty}^t y dt'$ where y is a function of t we can write the differential equation $\frac{dy}{dt} + ay = x$ as $py + ay = x$.

Algebraically this can be written as $y(p + a) = x$, giving $y = \frac{1}{p+a}x$ where $\frac{1}{p+a}$ can be thought of as an operator acting on the function x to give the function y as an output.

Taking $p[e^{at}y]$ we have,

$$p[e^{at}y] = ae^{at}y + e^{at}py = e^{at}(p + a)y$$

Returning to the expression $y(p + a) = x$ we can multiply both sides of this equation by e^{at} to give

$$e^{at}y(p + a) = e^{at}x$$

Therefore

$$p[e^{at}y] = e^{at}x$$

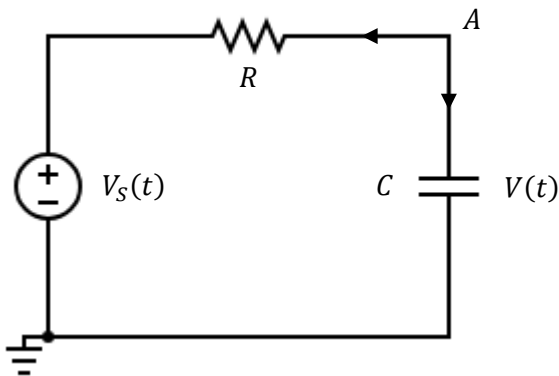
Given that p and $\frac{1}{p}$ are inverse operations

$$e^{at}y = \frac{1}{p}[e^{at}x]$$

Which gives y as

$$y = e^{-at} \frac{1}{p}[e^{at}x]$$

RC Circuit



The algebraic sum of currents meeting at node A is zero, the current passing through the resistor being $\frac{V(t) - V_S(t)}{R}$ while the current passing through the capacitor is $C \frac{dV}{dt}$.

Therefore,

$$\frac{V - V_S}{R} + C \frac{dV}{dt} = 0$$

Dividing both sides by C and moving $\frac{1}{RC}V_S$ to the other side of the equation we have

$$\frac{dV}{dt} + \frac{1}{RC}V = \frac{1}{RC}V_s$$

This is now in the form of the differential equation previously encountered and solved, $py + ay = x$. Where y is V , a is $\frac{1}{RC}$ and x is $\frac{1}{RC}V_s$.

In order to model the response, $V(t)$ of the above circuit when a constant voltage V_m is applied at $t = 0$ we can let $V_s = u(t)V_m$ where $u(t)$ is the unit step function.

To model the response once a constant voltage of V_m is removed from the circuit when $t = 0$ we can let $V_s = (1 - u(t))V_m$.

$$V = e^{-\frac{t}{RC}} \frac{1}{p} \left[e^{\frac{t}{RC}} \frac{1}{RC} u(t)V_m \right] = e^{-\frac{t}{RC}} \int_{-\infty}^t e^{\frac{t'}{RC}} \frac{1}{RC} u(t')V_m dt'$$

Given the function being integrated has a value of zero when $t < 0$ we can integrate from 0 to t and bring $u(t)$ out of the integral. Bringing out the other constants $\frac{1}{RC}$ and V_m we have

$$\begin{aligned} V &= u(t) \frac{V_m}{RC} e^{-\frac{t}{RC}} \int_0^t e^{\frac{t'}{RC}} dt' = u(t) \frac{V_m}{RC} e^{-\frac{t}{RC}} \left[RC e^{\frac{t'}{RC}} \right]_0^t = u(t) \frac{V_m}{RC} e^{-\frac{t}{RC}} \left[RC e^{\frac{t}{RC}} - RC \right] \\ &= u(t)V_m e^{-\frac{t}{RC}} \left[e^{\frac{t}{RC}} - 1 \right] = u(t)V_m \left[1 - e^{-\frac{t}{RC}} \right] \end{aligned}$$

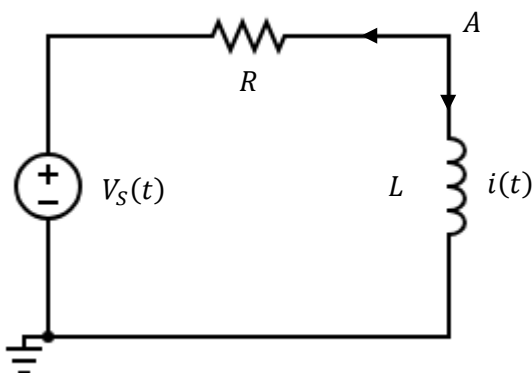
Letting $V_s = (1 - u(t))V_m$ we have,

$$V = e^{-\frac{t}{RC}} \frac{1}{p} \left[e^{\frac{t}{RC}} \frac{1}{RC} (1 - u(t))V_m \right] = e^{-\frac{t}{RC}} \int_{-\infty}^t e^{\frac{t'}{RC}} \frac{1}{RC} (1 - u(t'))V_m dt'$$

Now the function being integrated has a value of zero when $t > 0$, therefore it becomes pointless to integrate past zero. Additionally, because we are only interested in what happens after $t = 0$ we can decide to integrate from $-\infty$ to 0. $(1 - u(t))$ has a value of one when t is between $-\infty$ and 0, therefore when integrating from $-\infty$ to 0, $(1 - u(t))$ can be removed from the integral. Taking out the constants $\frac{1}{RC}$ and V_m we have

$$V = \frac{V_m}{RC} e^{-\frac{t}{RC}} \int_{-\infty}^0 e^{\frac{t'}{RC}} dt' = \frac{V_m}{RC} e^{-\frac{t}{RC}} \left[RC e^{\frac{t'}{RC}} \right]_{-\infty}^0 = \frac{V_m}{RC} e^{-\frac{t}{RC}} [RC] = V_m e^{-\frac{t}{RC}}$$

RL Circuit



Again, the algebraic sum of currents meeting at node A is zero. The current passing through the inductor being $i(t)$, the current passing through the inductor can be found as $\frac{L}{R} \frac{d}{dt} i(t) - \frac{1}{R} V_S(t)$ given that the voltage across the inductor is $L \frac{di}{dt}$.

We have

$$\frac{L}{R} \frac{di}{dt} - \frac{1}{R} V_S + i = 0$$

Multiplying by R and dividing by L , as well as moving $\frac{1}{L} V_S$ to the other side of the equation we have

$$\frac{di}{dt} + \frac{R}{L} i = \frac{1}{L} V_S$$

This being written in the form $py + ay = x$ where y is i , a is $\frac{R}{L}$ and x is $\frac{1}{L} V_S$.

To model the currents response in the circuit to the application and removal of a constant voltage V_m at the point $t = 0$, we can use $V_S = u(t)V_m$ for application and $V_S = (1 - u(t))V_m$ for removal.

$$\begin{aligned} i &= e^{-\frac{Rt}{L}} \frac{1}{p} \left[e^{\frac{Rt}{L}} \frac{1}{L} u(t) V_m \right] = e^{-\frac{Rt}{L}} \int_{-\infty}^t e^{\frac{Rt'}{L}} \frac{1}{L} u(t') V_m dt' = u(t) \frac{V_m}{L} e^{-\frac{Rt}{L}} \int_0^t e^{\frac{Rt'}{L}} dt' \\ &= u(t) \frac{V_m}{L} e^{-\frac{Rt}{L}} \left[\frac{L}{R} e^{\frac{Rt'}{L}} \right]_0^t = u(t) \frac{V_m}{L} e^{-\frac{Rt}{L}} \left[\frac{L}{R} e^{\frac{Rt}{L}} - \frac{L}{R} \right] = u(t) \frac{V_m}{R} e^{-\frac{Rt}{L}} \left[e^{\frac{Rt}{L}} - 1 \right] \\ &= u(t) \frac{V_m}{R} \left[1 - e^{-\frac{Rt}{L}} \right] \end{aligned}$$

In this circuit the inductor resists change in the current once the voltage V_m is applied, as t approaches infinity the current $i(t)$ approaches its maximum values I_{Max} which is $\frac{V_m}{R}$, therefore $i(t)$ can be written as

$$i = u(t) I_{Max} \left[1 - e^{-\frac{Rt}{L}} \right]$$

Letting $V_S = (1 - u(t))V_m$

$$\begin{aligned} i &= e^{-\frac{Rt}{L}} \frac{1}{p} \left[e^{\frac{Rt}{L}} \frac{1}{L} (1 - u(t)) V_m \right] = e^{-\frac{Rt}{L}} \int_{-\infty}^t e^{\frac{Rt'}{L}} \frac{1}{L} (1 - u(t')) V_m dt' = \frac{V_m}{L} e^{-\frac{Rt}{L}} \int_{-\infty}^0 e^{\frac{Rt'}{L}} dt' \\ &= \frac{V_m}{L} e^{-\frac{Rt}{L}} \left[\frac{L}{R} e^{\frac{Rt'}{L}} \right]_{-\infty}^0 = \frac{V_m}{L} e^{-\frac{Rt}{L}} \left[\frac{L}{R} \right] = \frac{V_m}{R} e^{-\frac{Rt}{L}} \end{aligned}$$

Given that $I_{Max} = \frac{V_m}{R}$

$$i = I_{Max} e^{-\frac{Rt}{L}}$$